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# **Titanium Oxynitride Thin Films Wide Temperature Range Sensors**

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The temperature dependence of the resistivity of titanium oxynitride  $\text{TiN}_x \text{O}_y$  thin films with different oxygen and nitrogen content obtained by atomic layer deposition was investigated. We found that the resistance of all films monotonically decreased with increasing temperature and varied within a wide range depending on the chemical composition and thickness of the film. The technology for obtaining a compact temperature sensor of wide range from helium to room temperature based on 40 nm thick  $\text{TiN}_{0.87}\text{O}_{0.97}$  is presented.

Keywords: titanium oxide-nitride, temperature sensors, thin films, atomic layer deposition, integrated circuit components.

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Thin-film titanium oxynitride  $TiN_xO_y$  is used widely in various devices, such as integrated resistors [1], capacitors with a metal-insulator-metal structure (MIM capacitors) [2], photocatalysts [3,4], solar selective absorbers [5,6], and efficient photovoltaic energy converters [7]. The application of  $TiN_xO_y$  films as temperature sensors with a wide operating range is a new field of use of this material. Cernox<sup>TM</sup> sensors based on zirconium oxynitride [8], carbon glasses, ruthenium oxide, and germanium tunnel diodes [9] are a well-known solution in this field. In the present study, we propose a novel method for fabrication of such sensors with the use of thin  $TiN_xO_y$  films fabricated by atomic layer deposition (ALD). The method of reactive magnetron sputtering is the one commonly used for titanium oxynitride synthesis [10]. However, ALD has an advantage in that it offers a considerably better thickness uniformity and a lower resistivity of grown films [7,11].

Films were grown in a SUNALE<sup>TM</sup> R-200 ADVANCED (Picosun Oy, Finland) system without a load lock chamber at a temperature of 420°C. Two types of films with an increased (*G*1) and a reduced (*G*2) oxygen content were obtained. Liquid titanium tetrachloride (TiCl<sub>4</sub>, 5N purity), gaseous ammonia (NH<sub>3</sub>, 6N), and residual oxygen in the ALD chamber served as the sources of titanium, nitrogen, and oxygen, respectively. Sitall ST-32-1 plates with a thickness of 500  $\mu$ m and (100) Si wafers ( $\rho > 0.1 \text{ k}\Omega \cdot \text{m}$ ) with a thickness of 720  $\mu$ m were used as substrates. TiCl<sub>4</sub> and NH<sub>3</sub> were fed periodically into the chamber in alternating 0.1- and 1-s-long pulses, respectively. In each deposition cycle, TiCl<sub>4</sub> was purged with a 2.5  $\cdot 10^{-6} \text{ m}^3 \cdot \text{s}^{-1}$  flow of nitrogen (7N) for 2 s, while NH<sub>3</sub> was purged with

a flow of  $1.7 \cdot 10^{-6}$  m<sup>3</sup> · s<sup>-1</sup> for 4 s. The base pressure was 500–700 Pa. The maximum pressure of TiCl<sub>4</sub> and NH<sub>3</sub> pulses was as high as 2500–3000 and 4000–4500 Pa, respectively. Prior to the growth of the studied TiN<sub>x</sub>O<sub>y</sub> film samples, the ALD reactor chamber was purged with pure nitrogen (8N), annealed at 420°C for 4 h, and passivated in 2000 cycles of TiN<sub>x</sub>O<sub>y</sub> growth at 420°C. The concentration of oxygen in films G2 was reduced by purging the ALD chamber with forming gas (FG) (N<sub>2</sub> (5N):H<sub>2</sub>(6N)=97:3) immediately before the start of the growth process. FG was supplied for 900 s in pulses with a duration of 15 s without purging with nitrogen. The process parameters of TiN<sub>x</sub>O<sub>y</sub> growth were detailed in [12].

The film thickness was measured with a Hitachi HT7700 transmission electron microscope (TEM) at a voltage of 100 kV and an emission current of  $8 \mu A$  (Fig. 1, *a*). Figure 1 shows the TEM image of the  $TiN_{0.55}O_{0.95}$  film cross section. The SiO<sub>2</sub> layer below TiN<sub>0.55</sub>O<sub>0.95</sub> formed as a result of silicon oxidation in the process of loading a wafer into the hot ALD chamber and evacuation to the base vacuum. Roughness  $S_q$  (mean-square height) and the maximum level difference  $S_z$  of the obtained film texture was measured using atomic force microscopy (AFM) for samples type G1 and G2 (Figs. 1, b, c). The typical values of  $S_q$  for films G1 and G2 on sitall are 4.1 and 3.0 nm, and the values of  $S_z$  are 52 and 34 nm, respectively. Films grown on silicon have lower  $S_q$  (2.9 nm) and  $S_z$  (22 nm) values. TiN<sub>x</sub>O<sub>y</sub> films with a lower oxygen concentration have better-quality surfaces with a lower roughness.

The transport properties of films were determined using the four-probe method and a LakeShore EMPX-H2



**Figure 1.** a - TEM image of sample G2-Si-638 of thin-film TiN<sub>0.55</sub>O<sub>0.95</sub> on SiO<sub>2</sub>/Si synthesized by ALD. b, c - AFM data for the surface of titanium oxynitride films on sitall and histograms of the grain size distribution:  $b - \text{TiN}_{0.46}O_{1.52}$  with a high relative oxygen content,  $c - \text{TiN}_{0.87}O_{0.97}$  with a low relative oxygen content.

Sample	Ti, at.%	N, at.%	O, at.%	Formula	Film thickness, nm	$\rho, \Omega \cdot m$ (at 300 K)
G2-Si-638	40	22	38	TiN <sub>0.55</sub> O <sub>0.95</sub>	11	$7.8 \cdot 10^{-5}$
G1-Si-2000	33	16	51	TiN <sub>0.48</sub> O <sub>1.56</sub>	20	$(7.7 - 16) \cdot 10^{-4}$
G1-SIT-2000	34	15	51	TiN <sub>0.46</sub> O <sub>1.52</sub>	20	$(3.3 - 10) \cdot 10^{-4}$
G2-Si-4000	36	29	35	TiN <sub>0.81</sub> O <sub>0.98</sub>	90	$1.0 \cdot 10^{-5}$
G2-SIT-4000	35	31	34	TiN <sub>0.87</sub> O <sub>0.97</sub>	90	$9.0\cdot 10^{-6}$

Chemical composition and resistivity of TiN<sub>x</sub>O<sub>y</sub> films

cryogenic probe station. Measurements were performed with a Kiethley 2634B dual-channel sourcemeter in the direct current mode. The temperature dependences of resistivity of  $\text{TiN}_x \text{O}_y$  films were obtained this way. The composition of films and the chemical state of elements were determined by X-ray photoelectron spectroscopy using a SPECS (Germany) spectrometer with a PHOIBOS 150 MCD 9 hemispherical analyzer; prior to these measurements, the surface was cleaned by ion etching. Data on the composition and resistivity of several typical samples are presented in the table. The sample designations contain the following information: oxygen concentration group (*G*1 or *G*2), substrate material (silicon or sitall), and number of ALD growth cycles. The chemical composition of films was determined more accurately in regard to the copper concentration by Rutherford backscattering of helium  ${}^{4}\text{He}^{+}$ ions accelerated to 1.5 MeV in an AN2500 Van de Graaff accelerator produced by High Voltage Engineering Europa B.V. (Amersfoort, Netherlands). The obtained spectra were processed using the SIMNRA 7.03 program [13]. Although the FG supply line was fitted with a brass valve, TiN<sub>x</sub>O<sub>y</sub> films were not, in contrast to our previous experiments [12], contaminated with copper. The copper content did not exceed 0.02 at.%. The growth rate of *G*1 and *G*2 films was



**Figure 2.** Temperature dependences of resistivity of  $\text{TiN}_x \text{O}_y$  films deposited by ALD onto sitall plates (SIT) and silicon wafers (Si). The oxygen-to-nitrogen ratio in samples *G*1 is 2–3 times higher than the corresponding ratio in samples *G*2. Numbers in designations correspond to the total number of ALD growth cycles.

0.11 Å/cycle and 0.22 Å/cycle, respectively. The film growth rate decreases significantly when the oxygen concentration in the chamber increases.

Figure 2 presents the temperature dependences of resistivity of the studied  $TiN_xO_y$  films. All samples exhibit a strictly monotonic dependence of resistivity, which decreases with increasing temperature. The results of measurements at above-room temperature revealed that this monotonic resistivity reduction continues up to 260°C. At higher temperatures, the resistivity of group G1 films increases abruptly and irreversibly. Films G1 have a roughly inverse quadratic dependence on temperature, while the dependence for films G2 is hyperbolic. The range of resistivity variation depends on the thickness of films, the oxygen content, and the substrate roughness. It should be noted that films grown on a silicon substrate have a stronger temperature dependence in the low-temperature region. This is probably attributable to the difference in size of crystallites in films on silicon and sitall substrates (Fig. 1). Having analyzed the histograms of crystallite



Figure 3. Temperature dependence of resistance and photomicrograph (inset) of the sensor based on a  $TiN_{0.87}O_{0.97}$  film with a thickness of 40 nm.

size distributions, we found that the mean size of grains in films grown on sitall substrates is 140 nm for samples G1 and  $120 \,\mathrm{nm}$  for samples G2, while the corresponding value for samples G1 on silicon is 155 nm. The substrate roughness has a significant influence on resistivity (with the difference being as high as an order of magnitude) of thin films (11 nm), but has a less pronounced effect (50-100%)resistivity difference) in thick films (90 nm). Roughness  $S_q$ of the initial substrates determined based on AFM data was 0.28 nm for silicon and 16.76 nm for sitall. An increase (reduction) in oxygen (nitrogen) content and a reduction in the film thickness contribute to a significant (1-2 orders of magnitude) increase in resistivity. Indeed, it follows from the table that samples G2-Si-638 and G2-Si-4000 have very close oxygen concentrations, but differ in thickness by a factor of  $\sim 8.2$ , which is roughly equal to the inverse ratio of their resistivities ( $\sim 7.8$ ). Comparing samples G2-Si-4000 and G2-SIT-4000 with the same film thickness and different oxygen content, one also finds that a 1% reduction in oxygen concentration translates into a 10% reduction in resistivity.

Figure 3 presents the temperature dependence of resistance and the photomicrograph of a typical  $\text{TiN}_x \text{O}_y$  sensor with interconnections and contact pads with a gold coating. The body of this sensor was formed from a low-resistivity *G*2  $\text{TiN}_{0.87}\text{O}_{0.97}$  film with a thickness of 40 nm deposited onto sitall. The process of fabrication of this structure has been illustrated earlier through an example of resistive elements based on a *G*1  $\text{TiN}_{0.82}\text{O}_{1.43}$  film [14]. The active region (body) of the sensor was formed from a  $\text{TiN}_{0.87}\text{O}_{0.97}$  film by optical lithography in an EVG 610 setup with subsequent plasma etching in a RIE-1701 Nordson MARCH system in a CF<sub>4</sub> ( $2.5 \cdot 10^{-7}\text{m}^3 \cdot \text{s}^{-1}$ )/O<sub>2</sub> ( $5 \cdot 10^{-8}\text{m}^3 \cdot \text{s}^{-1}$ ) gas mixture at a high-frequency power of 250 W and a pressure 33 Pa for 120 s. Electric contacts and

interconnections were formed as a second overlapping layer by optical lithography with the use of an AZ nLOF-2035 negative photoresist and electron beam deposition of Ni (5 nm)/Cu (1  $\mu$ m)/Ni (5 nm)/Au (50 nm) with subsequent lift-off stripping in acetone.

This method of fabrication of temperature sensors provides an opportunity to adjust their resistance within a wide range  $(0.01-100 \text{ k}\Omega)$  by controlling accurately the thickness of  $\text{TiN}_x O_y$  in the process of ALD growth and the geometric size of the structure in lithography and by varying the oxygen content. We plan to establish control over the oxygen concentration parameter in the future. The sensor fabrication process is based on standard silicon microelectronics technology, and the obtained sensor itself is easy to integrate into modern microchips.

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### **Conflict of interest**

The authors declare that they have no conflict of interest.

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