# **Thermoelectric properties of Fe-V-Al Heusler alloy with excess of Al and deficiency of Fe**

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> The results of the experimental studies of the thermoelectric properties of a Fe1*.*68VAl1*.*<sup>32</sup> *p*-type Heuser alloy are presented. A comparison of the electrical resistivity  $\rho$  and the Seebeck coefficient *S* measured in a temperature range 300−475 K with data, published for other Fe-V-Al *p*-type with different chemical compositions, showed that  $Fe<sub>1.68</sub>VAL<sub>1.32</sub>$  has the lowest  $\rho$  and one of the highest values of *S*. This leads to one of the record values of the power factor value  $PF \approx 1.7 \text{ mW/(m}^{-1} \cdot \text{K}^{-2}$  (at  $T = 384 \text{ K}$ ) in Fe<sub>1.68</sub>VAl<sub>1.32</sub>, which is an order of magnitude higher than that in the stochiometric *PF*. The results of thermal conductivity measurements showed high values of  $\kappa$  ( $\approx$  11.11 W/(m<sup>-1</sup> · K<sup>-1</sup>)) in the studied compound, which is comparable to thermal conductivity of the stochiometric Fe<sub>2</sub>VAl.

**Keywords:** Heusler alloys, arc melting, transport properties, power factor.

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## **1. Introduction**

Heusler alloys are triple intermetallic compounds and are generally divided in two classes. The first type compounds, the so-called Full-Heusler alloys, are featuring  $X_2$ YZ stoichiometry and  $L2_1$  structural type of a cubic lattice. The second type compounds include the so-called Half-Heusler alloys with XYZ stoichiometry and  $Cl_b$  type of a cubic lattice. In both cases  $X$ ,  $Y$  elements — are transition metals of  $4-11$  groups, and  $Z$  — are the elements of the main group (Al, Ga, In, Si, Ge, Sn, Sb) [1].

Stability of Heusler alloys is mostly defined by the valence electron rule. So, for XYZ alloys is equal to 18, and for  $X_2$ YZ alloys — 24. Deviations from these values in most cases lead to instability of the compound. However, recently it was suggested [2], that due to the introduction of some defects it is possible to obtain Half-Heusler alloys with 18 valence electrons from the unstable compounds with 19 valence electrons. By using this approach the paper [3] describes the study of an alloy with a composition close to Fe1*.*25VAl — a non-stoichiometric Full-Heusler alloy with 18 valence electrons the number of which was corrected by introducing new vacancies.

Compared to Half-Heusler alloys, the thermoelectric Q-factor *z T* of Full-Heusler alloys is much lower [4]. Yet, Full-Heusler alloys, Fe<sub>2</sub>VAl in particular, attract a lot of interest from researchers because of the non-toxic nature and low cost of chemical elements in these alloys. Recent studies have demonstrated that a complex substitution of vanadium and aluminum positions in the stoichiometric Fe<sub>2</sub>VAl enables to increase  $zT$  up to  $\sim$  0.34 and obtain large values of the power factor  $\overrightarrow{PF} \approx 10 \text{ mW/(m}^{-1} \cdot \text{K}^{-2})$ in alloys of *n*-type of conductivity [5]. In addition, it was found that aluminum has high solubility in  $Fe<sub>2</sub>VAL$  [6]

compounds, that, by variating the component contents, may impact the thermoelectric properties of the initial compound and obtain larger power factor values for alloys of *p*-type of conductivity. The purpose of this paper  $-$  study the influence of iron deficiency on the thermoelectric properties of Fe2VAl alloy with excess aluminum.

# **2. Samples and measurement procedures**

Nominal composition alloy  $Fe_{42}V_{25}Al_{33}$  (at%) was obtained in the electric-arc furnace using pure (Fe  $-$  99.99%,  $V - 99.93\%,$  Al  $- 99.99\%$  chemical elements. Weight loss in melting didn't exceed 0.2%. The fabricated ingot was placed in a quartz tube and annealed in the tubular furnace at a temperature of 1073 K during 120 h, after that the ingot was quenched in cold water. The annealed ingot was mechanically grinded in a mortar bowl. Later, by means of spark-plasma sintering (SPS), samples were fabricated from the powder to measure the thermoelectric properties. SPS was carried out in vacuum at 1273 K, compaction pressure of 65 MPa, and heating and cooling rates of 30 and 50◦C/min, respectively.

X-ray diffraction analysis was carried out at a room temperature on Difrey 401 diffractometer with Cr*Kα*-emission  $(\lambda = 2.2909 \text{ Å})$ . The microstructure and chemical composition were analyzed using scanning electron microscope (SEM) Tescan Vega 3SB, with an integrated energydispersive X-ray spectrometry (EDS) unit. Thermal conductivity  $\kappa$  was calculated from the measured temperature dependence of the temperature diffusivity factor *χ*, obtained by laser flashing on laser unit Netzsch LFA 447, and using formula  $κ = C_p dχ$ , where  $C_p$  — specific heat capacity calculated theoretically according to Debye model, *d* density defined by hydrostatic weighing method. Electrical resistivity *ρ* and Seebeck coefficient *S* were measured on Cryotel unit by four-probe and differential methods, respectively.

#### **3. Results and discussion**

The results of X-ray diffraction analysis are given in Figure 1. As seen from the observed reflections it may be concluded that the sample has a cubic lattice peculiar to these compounds with a parameter of  $a = 0.5815$  nm, which is slightly higher than for stoichiometric  $Fe<sub>2</sub>VAL$  $(a = 0.5762 \text{ nm})$  [7,8]. The absence of superstructure reflections (e.g., (111)) indicates that the studied alloy  $Fe<sub>1.68</sub>VAL<sub>1.32</sub>$  doesn't have a structure ordering of  $L2<sub>1</sub>$  type which is peculiar to the fully ordered Heusler alloys  $X_2$ YZ, but is crystallized into a partially disordered structure of B2 type, where V/Al sub-lattice is disordered [1]. The reflections from secondary phases on the diffraction pattern are not observed, which, given the device sensitivity, indicates that if they are present their volume fraction will be *<* 5%.

The analysis of microstructure images obtained using SEM method indicates that, apart from the ground phase, there's also a small amount of secondary phase present in the sample in the form of dendrite inclusions. Real chemical composition of a sample defined by ED in several points of the sample's grinded surface was found to be equal  $Fe_{42.1}V_{24.2}Al_{33.7}$  (at%), which is close to the chemical composition (Fe<sub>42</sub>V<sub>25</sub>Al<sub>33</sub>). It is not possible to determine the chemical composition by the same method because of very small (several  $\mu$ m) sizes of inclusions of this phase.

Temperature dependences of electrical resistivity *ρ* and Seebeck coefficient *S* are given in Figure 2. From Figure 2, *a* we may see that in the measured temperature range the



**Figure 1.** Diffraction pattern of Fe<sub>1.68</sub>VAl<sub>1.32</sub>.



**Figure 2.** Temperature dependence of electric resistivity (*a*) and Seebeck coefficient (*b*) at  $Fe<sub>1.68</sub>VAL<sub>1.32</sub>$  (*I*). Data from literature for Fe<sub>2</sub>VAl (2) [7], Fe<sub>2.08</sub>V<sub>0.92</sub>Al (3) [8], Fe<sub>2</sub>VAl<sub>1.2</sub>, Fe<sub>2</sub>VAl<sub>1.6</sub> and Fe2VAl<sup>2</sup> (*4*−*6*), respectively, are given for comparison [6].

dependence  $\rho(T)$  in Fe<sub>1.68</sub>VAl<sub>1.32</sub> is featuring a semiconducting nature going down from  $\rho \approx 650 \,\mu\text{Ohm} \cdot \text{cm}$  at room temperature to  $\rho \approx 320 \,\mu\text{Ohm} \cdot \text{cm}$  at  $T = 475 \,\text{K}$ . It should be noted that semiconducting nature of electrical resistivity is typical at  $T > 300$  K both, in non-doped [3–5], and doped alloys [9,10] of Fe-V-Al system. By comparing the values  $\rho$  in the studied alloy with the values measured for the stoichiometric Fe2VAl (curve *2*), Fe-V-Al with excessive Fe (curve *3*) and with excessive Al (curves *4*−*6*), we may see that Fe<sub>1.68</sub>VAl<sub>1.32</sub> has the lowest electrical resistivity among all presented materials at temperatures of  $>$  310 K. At lower temperatures the values  $\rho$  in our sample exceed the values  $\rho$  in Fe<sub>2</sub>VAl<sub>2</sub>, the electrical resistivity of which demonstrates behavior typical for metals up to  $T = 4K$  [6]. Small values of electrical resistivity in  $Fe<sub>1.68</sub>VAL<sub>1.32</sub>$  may be due to the increase of the charge carriers concentration (holes in our case, as shown below) when Fe is substituted by Al.



**Figure 3.** Temperature dependence of power factor in Fe1*.*68VAl1*.*32. For comparison literature data for other semiconductors of *p*-type are given: Fe<sub>2</sub>VAl (2) [7], Fe<sub>2.08</sub>V<sub>0.92</sub>Al (3) [8], Fe<sub>2</sub>VAl<sub>1</sub><sub>2</sub>, Fe<sub>2</sub>VAl<sub>1</sub><sup>6</sup> and Fe<sub>2</sub>VAl<sub>2</sub> ( $4-6$ ) respectively [6].



**Figure 4.** Temperature dependence of thermal conductivity in Fe<sub>1.68</sub>VAl<sub>1.32</sub>. Data from literature for Fe<sub>2</sub>VAl (2) [7], Fe<sub>2.08</sub>V<sub>0.92</sub>Al (3) [8], Fe<sub>2</sub>VAl<sub>1.2</sub>, Fe<sub>2</sub>VAl<sub>1.6</sub> and Fe<sub>2</sub>VAl<sub>2</sub> (4–6), respectively, are given for comparison [6].

The results of measuring the Seebeck coefficient *S* demonstrate that Fe<sub>1.68</sub>VAl<sub>1.32</sub> is itself a semiconductor of *p*-type (Figure 2, *b*). The temperature dependence *S* in Fe<sub>1.68</sub>VAl<sub>1.32</sub> is typical for the degenerated semiconductors. I. e. from Figure 2, *b* we may see that during heating at room temperature *S* is slightly growing in the beginning, reaching its maximal value  $S \approx 94 \mu\text{V/K}$  at  $T = 350 \text{ K}$ , and further it is going down with the following temperature growth. Fe2VAl semiconductor alloys generally demonstrate peak values on  $S(T)$  dependence [3,5], which is a consequence of a bipolar conductance representation. *S* values of the studied alloy are several times higher compared to the stoichiometric

 $Fe<sub>2</sub>VAL$  and to the alloy with excess of Fe, but lower than in some compounds with excess of Al (Figure 2, *b*).

Low values of electrical resistivity along with relatively high Seebeck coefficient result in large values of power factor *PF* (Figure 3). It should be noted that thermoelectric materials based on Fe2VAl of *n*-type demonstrate gigantic values of *PF* amounting to  $\sim 10 \text{ mW/(m}^{-1} \cdot \text{K}^{-2})$  [5], whereas in materials of *p*-type the power factor is much lower. For materials with this type of conductivity the record value  $PF = 1.9 \text{ mW/(m<sup>-1</sup> · K<sup>-2</sup>)}$  was achieved in alloy  $Fe<sub>2</sub>VAL<sub>1.6</sub>$  [6]. Comparison of power factors in materials based on Fe2VAl of *p*-type of conductivity shows (Figure 3) that power factor for Fe<sub>1.68</sub>VAl<sub>1.32</sub> studied in this paper is one of the largest ones reaching  $PF \approx 1.7 \,\text{mW/(m}^{-1} \cdot \text{K}^{-2})$ at  $T = 384$  K.

Temperature dependence of thermal conductivity *κ* in  $Fe<sub>1.68</sub>VAL<sub>1.32</sub>$  is shown in Figure 4. We may see that this alloy is characterized by high thermal conductivity which exceeds  $\kappa$  in stoichiometric Fe<sub>2</sub>VAl. Thermal conductivity Fe<sub>1.68</sub>VAl<sub>1.32</sub> is practically independent from temperature, and rises only from values of  $\kappa \approx 11.3 \text{ W/(m} \cdot \text{K)}$  at room temperature of up to  $\kappa \approx 12.2 \text{ W/(m} \cdot \text{K)}$  at  $T = 550 \text{ K}$ . Alloy  $Fe<sub>2</sub>VAL<sub>1,2</sub>$  studied in paper [6] with a slight excess of aluminum has similar values of thermal conductivity, while compounds with higher aluminum content demonstrate much lower values of *κ*.

## **4. Conclusion**

This paper outlines the study of thermoelectric properties of Heusler alloy Fe<sub>1.68</sub>VAl<sub>1.32</sub> which is featuring excess of aluminum and deficiency of iron as compared to the stoichiometric compound. Comparing the properties of this alloy with  $Fe<sub>2</sub>VAL$  alloys of other chemical compounds but of the same type of conductivity demonstrated that in the measured temperature interval  $Fe<sub>1.68</sub>VAL<sub>1.32</sub>$  has lowest values of electrical resistivity. This, apparently, is due to the rise of charge carriers concentration when Fe is substituted by Al. Along with this,  $Fe<sub>1.68</sub>VAL<sub>1.32</sub>$  demonstrates one of the largest Seebeck coefficient values allowing to reach the unprecedented power factor values. In spite of this, large values of thermal conductivity in Fe<sub>1.68</sub>VAl<sub>1.32</sub> didn't provide sufficient growth of thermoelectric Q factor *z T* for this material. However, given that sample of Fe<sub>1.68</sub>VAl<sub>1.32</sub> studied in this paper represented itself a coarse crystalline sintered powder, we may suggest that if crystallites are shrunk to sub-micron sizes the thermal conductivity of this sample can be significantly reduced and thus, *z T* can be increased.

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#### **Conflict of interest**

The authors declare that they have no conflict of interest.

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